



浙江大学电气工程学院

电机与拖动

主讲：卢琴芬

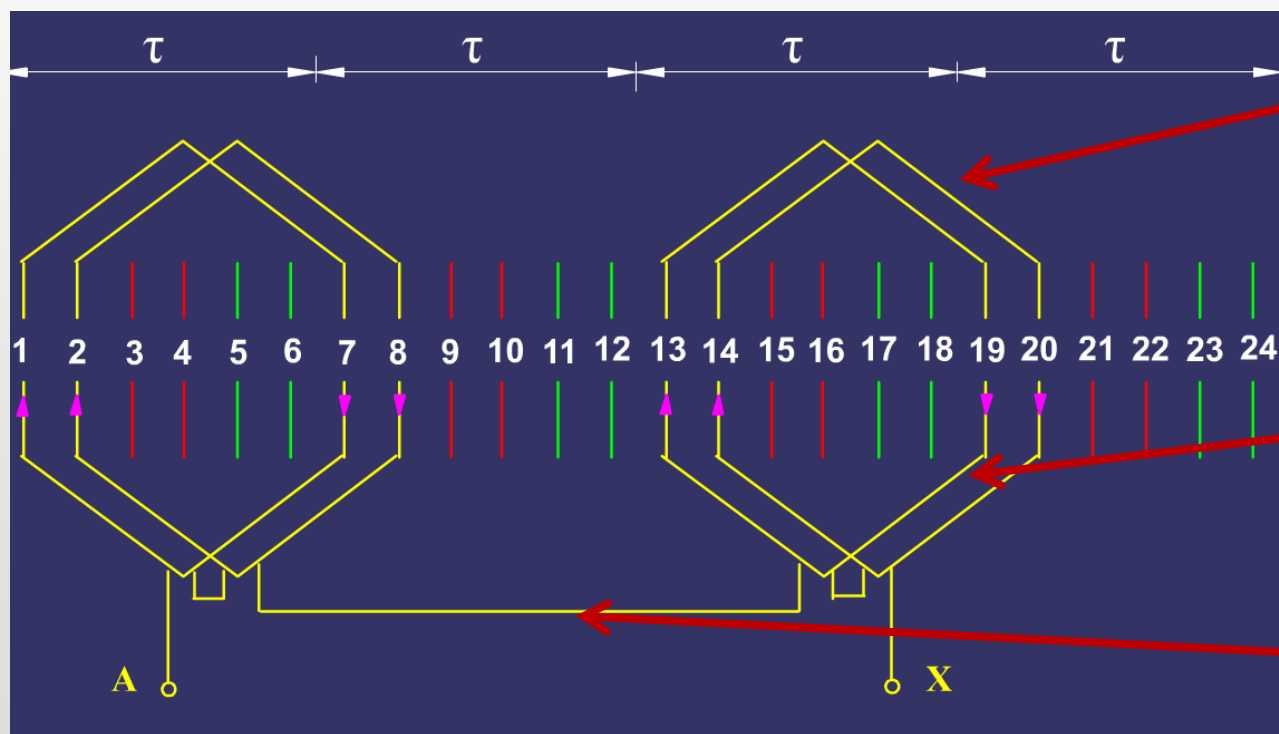
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交流绕组的感应电动势

磁场旋转

切割定子绕组 $\Rightarrow$ 定子绕组感应电动势

切割转子绕组
(若 n 不等于 n_1) $\Rightarrow$ 转子绕组感应电动势



单个(集中)绕组的基波电动势

线圈组的基波电动势

相绕组基波电动势

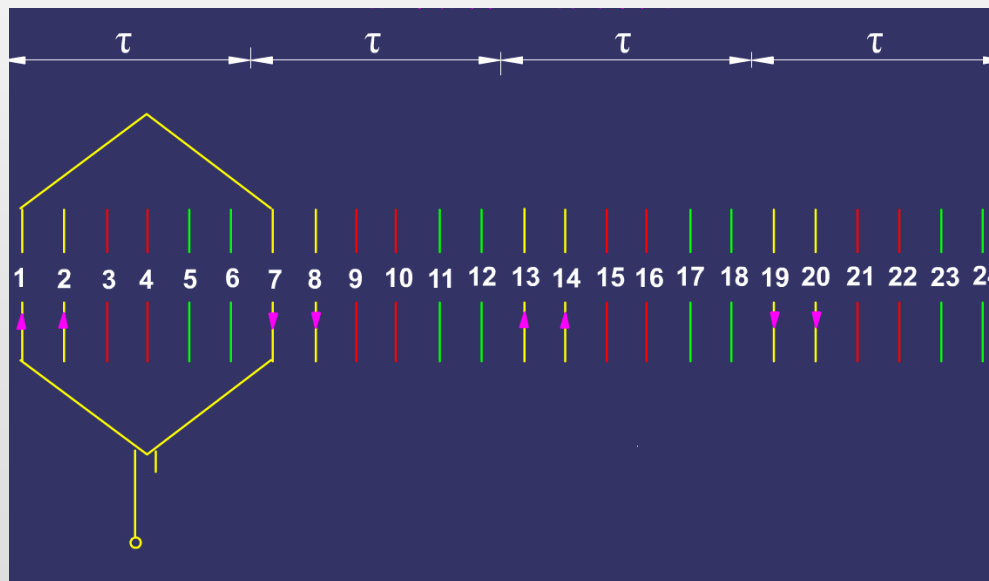
相绕组中的基波电动势

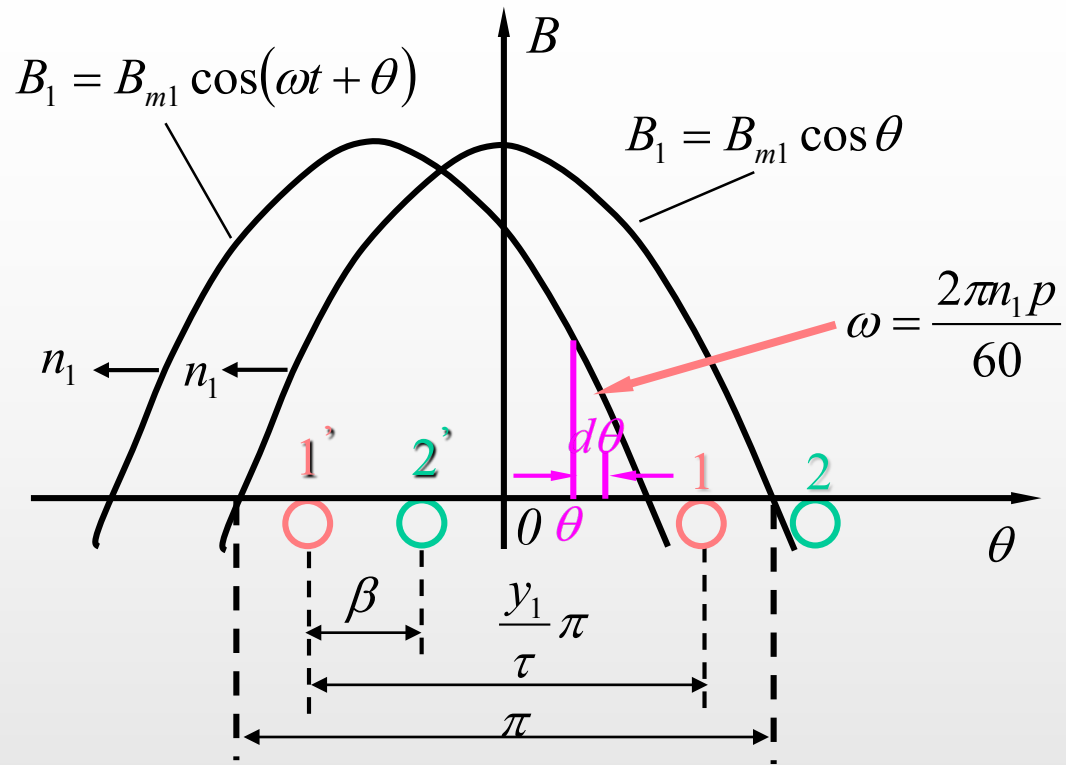
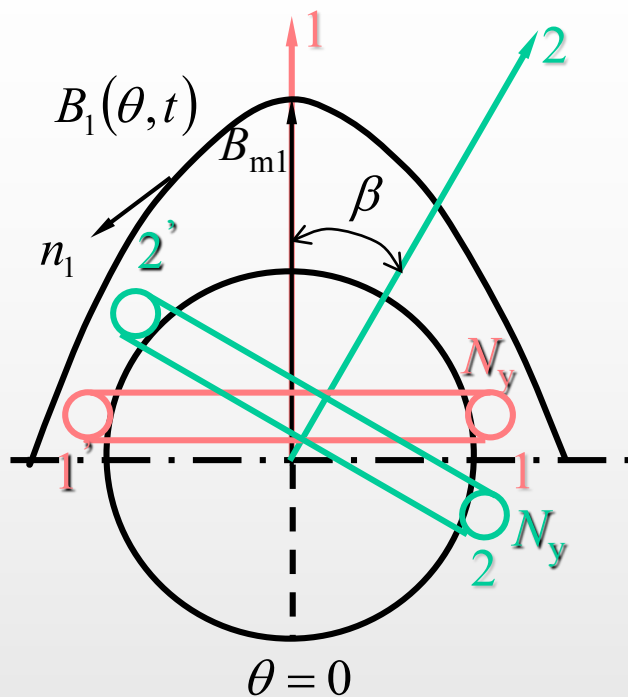
基波磁场:气隙磁场沿圆周正弦分布, 极数等于电动机的极数。

基波电动势:基波磁场在电机绕组中感应的电动势。

1.单个(集中)绕组的基波电动势

$$e_{y1} = -N \frac{d\Phi}{dt}$$





$$\phi_{11} = \int_{-\frac{y_1}{2\tau}}^{\frac{y_1}{2\tau}} B_{m1} \cos(\omega t + \theta) \cdot l \cdot \frac{\tau}{\pi} d\theta = \underbrace{\frac{2}{\pi} B_{m1} \cdot \tau l}_{\phi_1} \cdot \underbrace{\cos \omega t \cdot \sin \frac{y_1}{\tau} \frac{\pi}{2}}_{k_{y1}}$$

$$\phi_{11^c} = \int_{-\frac{y_1}{2\tau}}^{\frac{y_1}{2\tau}} B_{m_1} \cos(\omega t + \theta) \cdot l \cdot \frac{\tau}{\pi} d\theta = \underbrace{\frac{2}{\pi} B_{m_1} \cdot \tau l}_{\phi_1} \cdot \underbrace{\cos \omega t \cdot \sin \frac{y_1}{\tau} \frac{\pi}{2}}_{k_{y1}}$$

$$d\phi = B_1 l dx = B_{m_1} \cos(\omega t + \theta) \cdot l \cdot \frac{\tau}{\pi} d\theta = B_{m_1} \cdot \frac{\tau l}{\pi} \cos(\omega t + \theta) d\theta$$

$$e_{y1} = -N_y \frac{d\phi_{11^c}}{dt} = -N_y k_{y1} \frac{d\phi_1 \cos \omega t}{dt} = \underbrace{\omega \phi_1 N_y k_{y1}}_{E_{1m}} \sin \omega t = \sqrt{2} E_1 \cos(\omega t - 90^\circ)$$



$$E_1 = \frac{E_{1m}}{\sqrt{2}} = \frac{\omega \phi_1 N_y k_{y1}}{\sqrt{2}} = \frac{2\pi f \cdot \phi_1 N_y k_{y1}}{\sqrt{2}} = 4.44 f N_y k_{y1} \phi_1$$

$$\phi_{22^c} = \int_{-(\frac{y_1}{2\tau}-\beta)}^{\frac{y_1}{2\tau}\pi+\beta} B_{m1} \cos(\omega t + \theta) \cdot l \cdot \frac{\tau}{\pi} d\theta = \underbrace{\frac{2}{\pi} B_{m1} \cdot \tau l}_{\phi_1} \cdot \underbrace{\cos(\omega t + \beta) \cdot \sin \frac{y_1}{\tau} \frac{\pi}{2}}_{k_{y1}}$$

ϕ_1

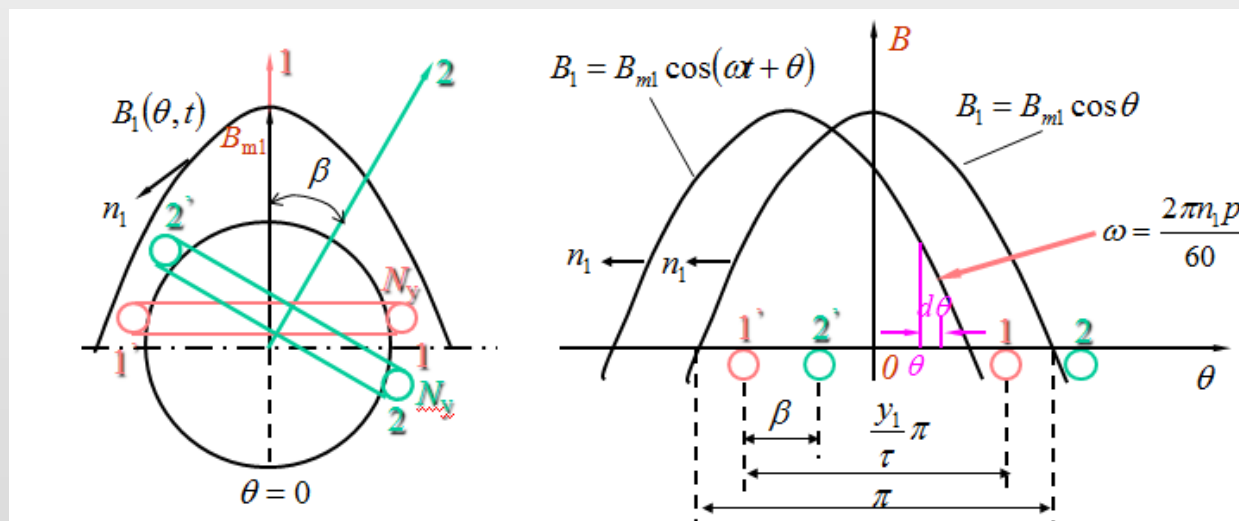
k_{y1}

$$e_{y2} = -N_y \frac{d\phi_{22^c}}{dt} = -N_y k_{y1} \frac{d\phi_1 \cos(\omega t + \beta)}{dt} = \omega \phi_1 N_y k_{y1} \sin(\omega t + \beta) = \sqrt{2} E_1 \cos(\omega t + \beta - 90^\circ)$$

$$e_{y1} = \sqrt{2} E_1 \cos(\omega t - 90^\circ)$$

$$E_1 = \frac{E_{1m}}{\sqrt{2}} = \frac{\omega \phi_1 N_y k_{y1}}{\sqrt{2}} = \frac{2\pi f \cdot \phi_1 N_y k_{y1}}{\sqrt{2}} = 4.44 f N_y k_{y1} \phi_1$$

E_{1m}



总结

(1) 感应电动势的频率与旋转磁场的频率相同

$$f_1 = \frac{pn_1}{60}$$

(2) 感应电动势的有效值

短距绕组

$$E_{y1} = \sqrt{2}\pi f_1 N_{y1} k_{y1} \Phi_1 \approx 4.44 f_1 N_{y1} k_{y1} \Phi_1$$

线圈的匝数

$$k_{y1} = \sin\left(\frac{y_1}{\tau} 90^\circ\right)$$

短距系数

整距绕组 $E_{y1} = \sqrt{2}\pi f_1 N_{y1} \Phi_1 \approx 4.44 f_1 N_{y1} \Phi_1$ 与变压器相同

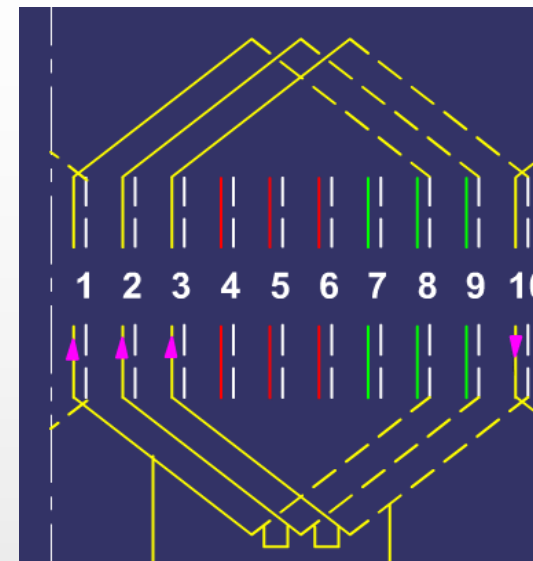
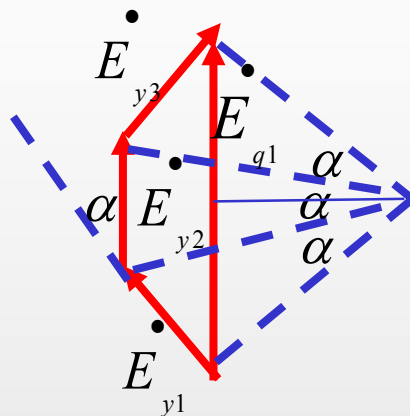
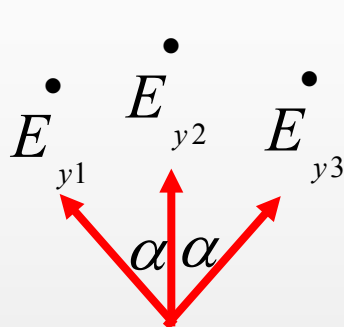
(3) 线圈在电枢的位置不同时，感应电动势有相位差。

$$e_{y1} = \sqrt{2}E_1 \cos(\omega t - 90^\circ)$$

$$e_{y2} = \sqrt{2}E_1 \cos(\omega t + \beta - 90^\circ)$$

线圈组的基波电动势

由 q 个 N_{y1} 相同的线圈，空间上互差 α 角个线圈组成



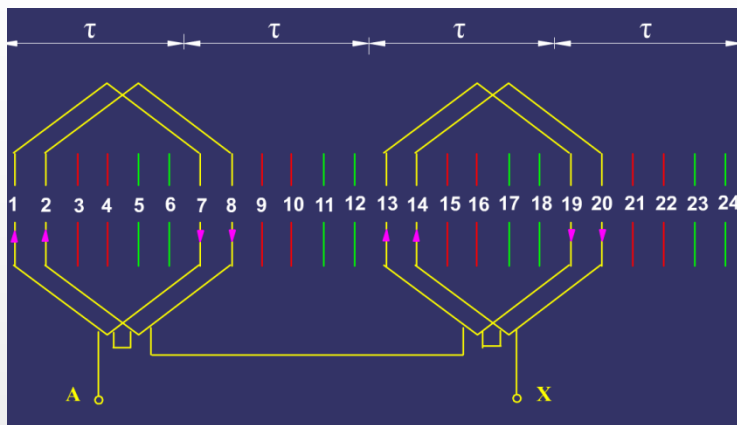
$$\begin{aligned} E_{q1} &= 2R \sin \frac{q\alpha}{2} \\ E_{y1} &= 2R \sin \frac{\alpha}{2} \end{aligned} \Rightarrow \frac{E_{q1}}{E_{y1}} = \frac{\sin \frac{q\alpha}{2}}{\sin \frac{\alpha}{2}} \Rightarrow E_{q1} = qE_{y1} \frac{\sin \frac{q\alpha}{2}}{q \sin \frac{\alpha}{2}} = qE_{y1} k_{q1}$$

分布系数

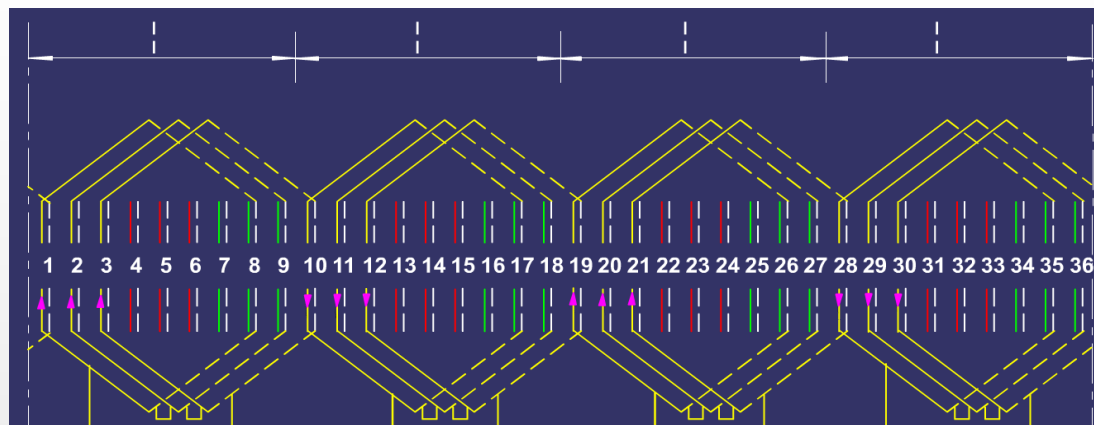
$$k_{q1} = \frac{q \text{ 个分布线圈线圈基波电动势矢量和}}{q \text{ 个分布线圈线圈基波电动势代数和}} < 1$$

相线圈的基波电动势

每相绕组由 $2p$ (双层)或 p 个(单层)线圈组而成。



$$E_{q1} = qE_{y1}k_{q1}$$



$$E_{\Phi 1}$$

$$E_{\Phi 1} = E_{q1} \frac{2p}{a} = \frac{2p}{a} qE_{y1}k_{q1} = 4.44 f_1 N_1 k_{w1} \Phi_1$$

双层绕组每相串联匝数 $N_1 = \frac{2p}{a} qN_{y1}$

单层绕组每相串联匝数 $N_1 = \frac{p}{a} qN_{y1}$

$k_{w1} = k_{q1}k_{y1}$
基波电动势
绕组系数

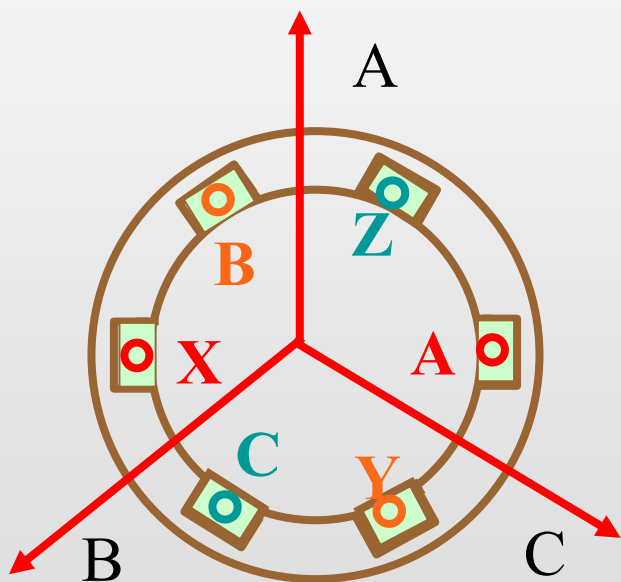
$$E_{\phi 1} = 4.44 f_1 \Phi_1 (N_1 k_{w1})$$

相绕组的基波电动势

$$E_{y1} = 4.44 f_1 \Phi_1 N_{y1}$$

单个整距的基波电动势

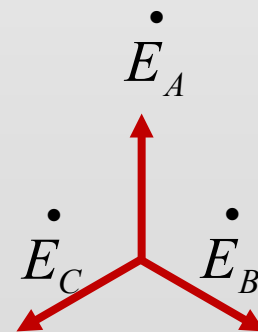
一个分布短距的实际相绕组 基波电动势相等 一个匝数为 $N_1 k_{w1}$ 的单个整距线圈
等效



A、B、C三相线圈有效匝数 $N_1 k_{w1}$ 相同，相位互差120电角度，同一个基波旋转磁场在三相绕组中产生的基波电动势大小相等，频率相同，相位互差120度，互相对称

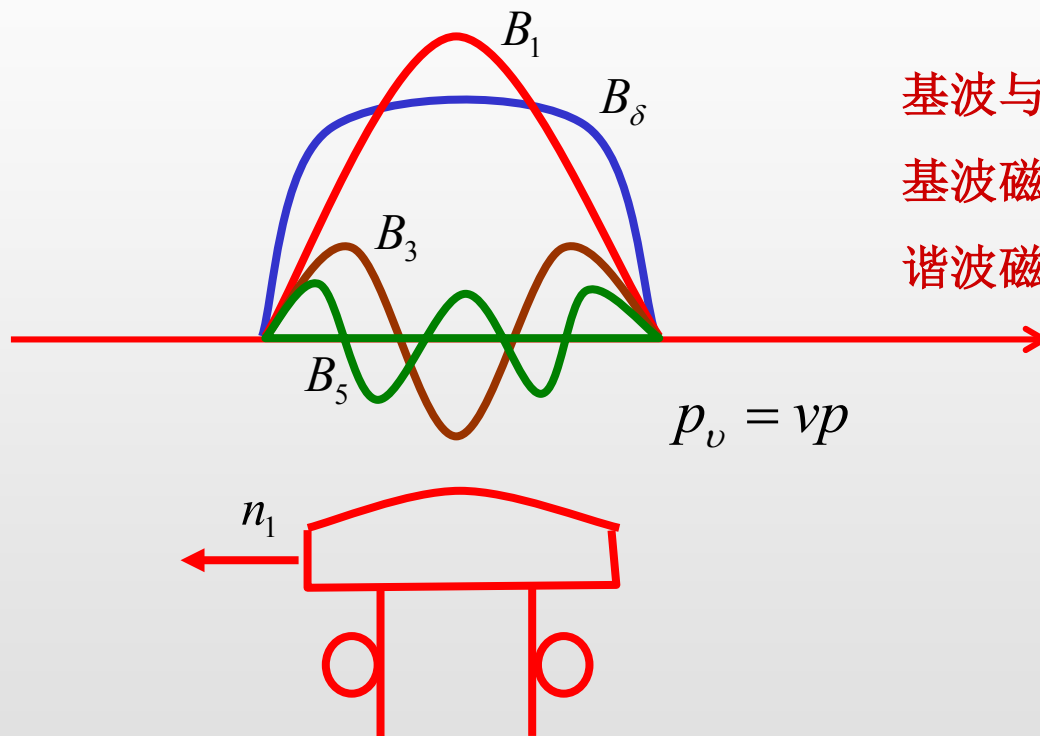
$$E_A = E_B = E_C = 4.44 f_1 N_1 k_{w1} \Phi_1$$

$$f = \frac{pn_1}{60}$$



相绕组中的谐波电动势

实际电机中，定转子铁芯表面开槽及同步电机的磁极形状等原因，气隙中的磁场沿圆周并非按正弦规律分布。



基波与谐波都要切割定子绕组，产生感应电动势，
基波磁场产生的感应电动势为基波电动势，
谐波磁场产生的感应电动势为谐波电动势。

$$\text{频率 } f_v = \frac{vp n_1}{60} = v f_1$$

$$\text{大小 } E_v = 4.44 f_v N_1 k_{wv} \Phi_v$$

$$k_{yv} = \sin\left(v \frac{y}{\tau} 90^\circ\right); k_{qv} = \frac{\sin\left(v \frac{q\alpha}{2}\right)}{q \sin \frac{v\alpha}{2}}$$
$$\Phi_v = \frac{2}{\pi} B_{mv} \tau_v l = \frac{2}{\pi} B_{mv} \frac{\tau}{v} l$$

削弱的方法：

合理设计同步电机的磁极形状、

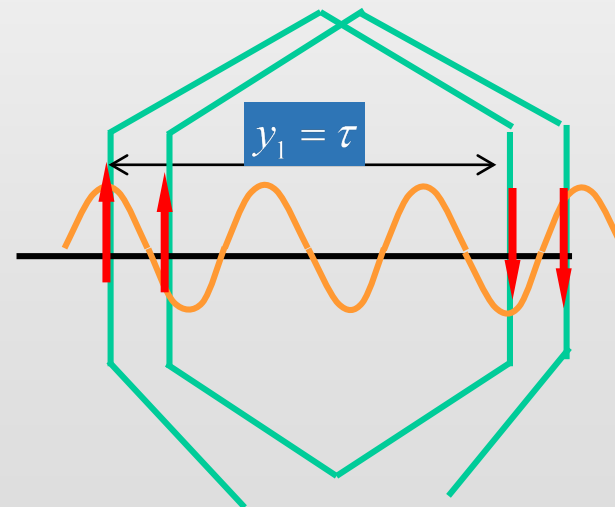
斜槽（感应电机）或斜极（同步电机）减小齿槽效应、

Y或 Δ 接法，消除线电动势中3倍次谐波电动势

分布短距（双层）。

采用分布绕组削弱高次谐波电动势。

$$\begin{matrix} q = 2 \\ \alpha = 30^\circ \end{matrix} \rightarrow \begin{cases} k_{q1} = 0.966 \\ k_{q5} = 0.2588 \\ k_{q7} = -0.2588 \end{cases}$$



采用绕组短距削弱高次谐波电动势。

$$\frac{y_1}{\tau} = \frac{5}{6} \rightarrow k_{y1} = 0.966, k_{y5} = 0.2588, k_{y7} = 0.2588$$

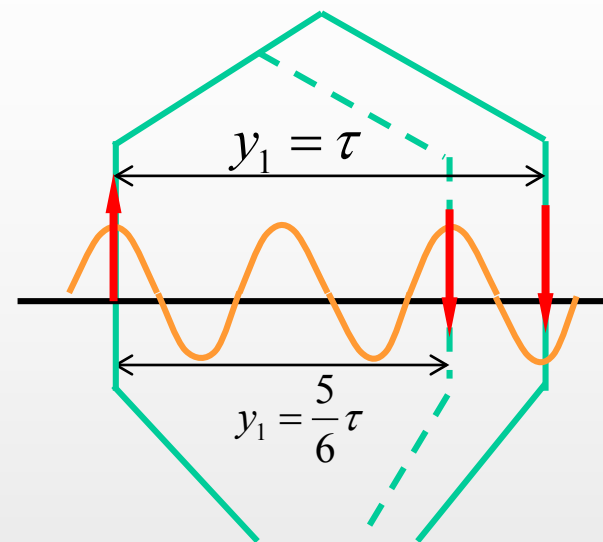
→ 消除 5 次、7 次谐波

$$\frac{y_1}{\tau} = \frac{7}{9} \rightarrow k_{y1} = 0.94, k_{y5} = -0.174, k_{y7} = 0.766$$

→ 消除 5 次谐波

$$\frac{y_1}{\tau} = \frac{8}{9} \rightarrow k_{y1} = 0.985, k_{y5} = 0.643, k_{y7} = -0.342$$

→ 削弱 7 次谐波



分布短距

基波电动势受到削弱，但影响不大
谐波电动势受到很大的削弱(5,7)

基本为正弦波



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T H A N K S

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